Uncertainty Analysis of the Thunder Scientific Model 2900 Two-Pressure Humidity Generator

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1.0 Introduction

Described here is the generated humidity uncertainty analysis, following the Guidelines of NIST and NCSL International ^[1, 6, 7], for a Model 2900 Humidity Generator that utilizes the NIST developed and proven two-pressure humidity generation principle ^[2, 3]. Generation of humidity in a system of this type does not require direct measurements of the water vapor content of the gas. Rather, the generated humidity is derived from the measurements of saturation and chamber pressures, and saturation and chamber temperatures.

The measurement instrumentation used in both our in-house working standards and our manufactured devices are obtained from companies which have demonstrated either NIST traceability or traceability to other acceptable standards. In most cases, we use the specifications supplied by these manufacturers as the starting point for our uncertainty statements. Over time, comparison calibrations against a NIST traceable pressure gauge and NIST traceable standard resistance thermometer, as well as the results of an on-going intercomparison program of both the individual components and of the outputs of generators as a system, have allowed the determination of the ranges of disagreement among the various temperatures and pressures that go into the final determination of the output uncertainties. The average values of these disagreements represent the uncertainties from our in-house processes and things like instrument drift over time; and these are coupled with the uncertainties given by the various instrument manufacturers to give overall uncertainty statements.

This document lists the various uncertainty sources, their magnitudes, and their origins over the operating range of the Model 2900 generator (refer to the specifications section in the Model 2900 system manual for exact operating range).

2.0 Defining Equations

NIST Technical Note 1297^[1] states that the uncertainty in a dependent variable, which depends only on uncorrelated input variables, is

$$u^{2}(y) = \sum_{i} u^{2}(x_{i}) \left(\frac{\partial y}{\partial x_{i}}\right)^{2}$$
⁽¹⁾

Relative Humidity is defined as the amount of water vapor in a sample compared to the maximum amount possible at the given sample's temperature and pressure.

This can be expressed by the following formula:

$$\% RH = \frac{e(T_D) \cdot f(T_D, P_C)}{e(T_C) \cdot f(T_C, P_C)} \cdot \eta_S$$
(2)

Where the *f* functions are enhancement factors, *e* is the saturation vapor pressure, η_s is the % efficiency of saturation, T_C is the chamber temperature, T_D is Dew/Frost point temperature, and Pc is the chamber pressure.

The Dew/Frost point temperatures can be expressed by the following formulas:

$$e_W(T_D) \cdot f(T_D, P_C) = f(T_S, P_S) \cdot e(T_S) \cdot \frac{P_C}{P_S}$$
⁽³⁾

$$e_I(T_F) \cdot f(T_F, P_C) = f(T_S, P_S) \cdot e(T_S) \cdot \frac{P_C}{P_S}$$
⁽⁴⁾

Where the *f* functions are enhancement factors, e_w is the saturation vapor pressure over water, e_I is the saturation vapor pressure over ice, T_D , T_F , T_S are the Dew point, Frost point and saturation temperatures, and Pc and Ps are the chamber and saturation pressures. Note that the actual Dew/Frost point temperature is defined implicitly and must be obtained through iterative solving.

Combining equation 2 with equations 3 and 4 we can express Relative Humidity in the terms of saturation and chamber temperatures and saturation and chamber pressure only by the following formula:

$$\% RH = \frac{e(T_s) \cdot f(T_s, P_s)}{e(T_c) \cdot f(T_c, P_c)} \cdot \frac{P_c}{P_s} \cdot \eta_s$$
⁽⁵⁾

By incorporating the relationship in equation 1 into an uncertainty equation of the form of equation 5, it can be shown that the total uncertainty in relative humidity is given by the expression:

$$u^{2}(RH) = u^{2}(T_{c})\left(\frac{\partial RH}{\partial T_{c}}\right)^{2} + u^{2}(T_{s})\left(\frac{\partial RH}{\partial T_{s}}\right)^{2} + u^{2}(P_{c})\left(\frac{\partial RH}{\partial P_{c}}\right)^{2} + u^{2}(P_{s})\left(\frac{\partial RH}{\partial P_{s}}\right)^{2} + u^{2}(\eta_{s})\left(\frac{\partial RH}{\partial \eta_{s}}\right)^{2}$$
(6)

Similarly incorporating the relationship in equation 1 into an uncertainty equation of the form of equation 3 and 4, the uncertainties in dew point and frost point measurement are given by the expression:

$$u^{2}(T_{D}) = u^{2}(T_{S}) \left(\frac{\partial T_{D}}{\partial T_{S}}\right)^{2} + u^{2}(P_{C}) \left(\frac{\partial T_{D}}{\partial P_{C}}\right)^{2} + u^{2}(P_{S}) \left(\frac{\partial T_{D}}{\partial P_{S}}\right)^{2} + u^{2}(\eta_{S}) \left(\frac{\partial T_{D}}{\partial \eta_{S}}\right)^{2}$$
(7)

and

$$u^{2}(T_{F}) = u^{2}(T_{S}) \left(\frac{\partial T_{F}}{\partial T_{S}}\right)^{2} + u^{2}(P_{C}) \left(\frac{\partial T_{F}}{\partial P_{C}}\right)^{2} + u^{2}(P_{S}) \left(\frac{\partial T_{F}}{\partial P_{S}}\right)^{2} + u^{2}(\eta_{S}) \left(\frac{\partial T_{F}}{\partial \eta_{S}}\right)^{2}$$
(8)

3 Uncertainty Components

In the mathematical analysis of equations 6, 7 and 8, we will analyze the uncertainties due to each component separately and then combine the uncertainties to obtain the total expanded uncertainty. We are concerned with four basic categories of uncertainty; pressure, temperature, the saturation vapor pressure/enhancement factor equations and percent efficiency of the saturator. Each of these categories may also have associated uncertainty components. In determining components of uncertainty, there are several things to consider, such as measurement accuracy or uncertainty, measurement resolution, uniformity, etc.

Listed below are the identified major uncertainty contributors and their components for the Model 2900 humidity generator.

- Uncertainty contribution from pressure (P_s and P_c) which includes
 - Measurement accuracy
 - Reference standard
 - o Linearity
 - o Drift
 - o Hysteresis
 - Temperature effects over the calibrated range
 - Repeatability
 - Measurement resolution
- Uncertainty contribution from temperature (T_s and T_c), which includes
 - Measurement accuracy
 - Reference standard
 - Measurement resolution
 - \circ Module error
 - o Hysteresis
 - o Self-Heating
 - Control Stability (Repeatability)
 - Chamber Uniformity (Applies to Chamber Temperature (T_c) only)
- Uncertainty contribution from Equations, which includes
 - Saturation Vapor Pressure Equation (e(T))
 - Enhancement Factor Equation (f(T,P))
- Uncertainty contribution from percent efficiency of the saturator (η_s)

3.1 Pressure Uncertainty Contribution

The pressure terms, P_c or P_s , in a two-pressure humidity generator are major determining factors. The Model 2900 humidity generator uses one pressure transducer to measure the saturation pressure and another pressure transducer to measure the chamber pressure. In this design, each pressure transducer contributes its own uncertainty to the overall system and will be addressed independent of one another.

The pressure uncertainty contribution in terms of relative humidity can be determined by the partial numeric differential of the RH equation with respect to pressure, multiplied by the uncertainty of the pressure component. The equation for this becomes.

$$uRH_{[component]} = \frac{\partial}{\partial P} \left[\frac{e_s(T_s) \cdot f(T_s, P_s)}{e_s(T_c) \cdot f(T_c, P_c)} \cdot \frac{P_c}{P_s} \cdot \eta_s \right] \cdot uP_{[component]}$$
(9)

uRH [component] = Pressure component uncertainty in terms of percent relative humidity.

uP_[component] = Pressure component uncertainty in terms of pressure.

The pressure uncertainty contribution in terms of dew or frost point temperature can be determined by the partial numeric differential of the iterative dew or frost point equation with respect to pressure, multiplied by the uncertainty of the pressure component. The equation for this becomes

$$\mathbf{uT}_{\mathrm{D[component]}} = \frac{\partial}{\partial P} \left[e_W(T_D) \cdot f(T_D, P) = f(T_S, P_S) \cdot e(T_S) \cdot \frac{P_C}{P_S} \right] \cdot \mathbf{uP}_{[\text{component]}}$$
(10)

$$\mathbf{u}\mathbf{T}_{\mathrm{F[component]}} = \frac{\partial}{\partial P} \left[e_I(T_F) \cdot f(T_F, P) = f(T_S, P_S) \cdot e(T_S) \cdot \frac{P_C}{P_S} \right] \cdot \mathbf{u}\mathbf{P}_{\mathrm{[component]}}$$
(11)

 $uT_{D[component]}$ = Pressure component uncertainty in terms of dew point temperature. $uT_{F[component]}$ = Pressure component uncertainty in terms of frost point temperature.

uP_[component] = Pressure component uncertainty in terms of pressure.

3.1.1 Pressure Accuracy Uncertainty Component

Pressure measurement accuracy of Model 2900 humidity generator's saturation pressure transducer is specified by the manufacturer as 0.02% of the full scale. This total manufacturer uncertainty (k=2) includes reference standard, linearity, drift, hysteresis, temperature effects over the calibrated range and repeatability. Taking a conservative approach that is based on a rectangular distribution, the uncertainty component of the saturation pressure accuracy is then

 $uP_{s[accuracy]} = (160 \text{ psia (full scale}) * 0.02\%) / \sqrt{3}$ = (0.032 psia) / \sqrt{3} (DOF=infinite)

Pressure measurement accuracy of Model 2900 humidity generator's chamber pressure transducer is specified by the manufacturer as 0.02% of reading. This total manufacturer uncertainty (k=2) includes reference standard, linearity, drift, hysteresis, temperature effects over the calibrated range and repeatability. Taking a conservative approach that is based on a rectangular distribution, the uncertainty component of the chamber pressure accuracy is then

$$uP_{c[accuracy]} = (14.7 \text{ psia (of reading)} * 0.02\%) / \sqrt{3}$$
$$= (0.00294 \text{ psia}) / \sqrt{3} (DOF=infinite)$$

Note: This analysis will use standard pressure as the chamber pressure reading for all calculations

3.1.2 Pressure Resolution Uncertainty Component

The Model 2900 humidity generator digitally communicates with both the saturation and chamber pressure transducers. Based on a rectangular distribution of the half-interval of resolution, the uncertainty component of pressure resolution is then

$$uP_{s \text{[resolution]}} = 0.001 \text{ psia} / \sqrt{12} \text{ (DOF=infinite)}$$

 $uP_{c \text{[resolution]}} = 0.001 \text{ psia} / \sqrt{12} \text{ (DOF=infinite)}$

3.1.3 Pressure Uncertainty Contribution Summary

The standard %RH uncertainties, uRH, components calculated using equation 9 from the associated individual pressure components are summarized in Table 1 and Figure 1.

			Standard	Pressure U	ncertainty	Componen	ts of RH (%	6)			
		5	Saturation	Pressure F	Range (psia	ı), Chambe	er pressure	= 14.7 psia	a	of n	u
Saturation	Description	15	20	30	40	50	75	100	150	rees	luatic
Temperature	-	98.0%RH	73.6%RH	49.2%RH	37.0%RH	29.6%RH	19.9%RH	15.0%RH	10.1%RH	Deg Fre	Eva
	Ps Accuracy	0.120280	0.067657	0.030069	0.016914	0.010824	0.004810	0.002706	0.001202	Infinity	Туре В
ပ္	Ps Resolution	0.001879	0.001057	0.000470	0.000264	0.000169	0.000075	0.000042	0.000019	Infinity	Туре В
0	Pc Accuracy	0.011277	0.008468	0.005659	0.004254	0.003412	0.002288	0.001726	0.001165	Infinity	Туре В
	Pc Resolution	0.000019	0.000014	0.000010	0.000007	0.000006	0.000004	0.000003	0.000002	Infinity	Туре В
	Combined	0.120822	0.068193	0.030601	0.017443	0.011351	0.005327	0.003210	0.001674	Infinity	
		98.0%RH	73.6%RH	49.1%RH	36.9%RH	29.6%RH	19.8%RH	14.9%RH	10.0%RH		
	Ps Accuracy	0.120373	0.067713	0.030096	0.016929	0.010835	0.004815	0.002708	0.001204	Infinity	Туре В
ပ္	Ps Resolution	0.001881	0.001058	0.000470	0.000265	0.000169	0.000075	0.000042	0.000019	Infinity	Туре В
35	Pc Accuracy	0.011286	0.008472	0.005658	0.004251	0.003407	0.002282	0.001719	0.001156	Infinity	Туре В
	Pc Resolution	0.000019	0.000014	0.000010	0.000007	0.000006	0.000004	0.000003	0.000002	Infinity	Туре В
	Combined	0.120915	0.068249	0.030627	0.017457	0.011359	0.005329	0.003208	0.001669	Infinity	
		98.0%RH	73.6%RH	49.2%RH	36.9%RH	29.6%RH	19.8%RH	14.9%RH	10.0%RH		
	Ps Accuracy	0.120218	0.067690	0.030114	0.016948	0.010850	0.004824	0.002714	0.001206	Infinity	Туре В
ပ္	Ps Resolution	0.001878	0.001058	0.000471	0.000265	0.000170	0.000075	0.000042	0.000019	Infinity	Туре В
70	Pc Accuracy	0.011270	0.008463	0.005653	0.004247	0.003403	0.002277	0.001714	0.001151	Infinity	Туре В
	Pc Resolution	0.000019	0.000014	0.000010	0.000007	0.000006	0.000004	0.000003	0.000002	Infinity	Туре В
	Combined	0.120759	0.068225	0.030644	0.017474	0.011372	0.005335	0.003210	0.001667	Infinity	

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Standard Pressure Uncertainty Components of RH (%)

Figure 1

The standard Dew Point Temperature uncertainties, uTD, components calculated using equation 10 from the associated individual pressure components are summarized in Table 2 and Figure 2.

		Standard	Pressure U	ncertainty	Componen	ts of Dew I	Point Temp	erature (•0	C)		
		S	Saturation	Pressure F	Range (psia	ı), Chambe	er pressure	= 14.7 psi	a	of a	u
Saturation	Description	15	20	30	40	50	75	100	150	rees	luatio
Temperature	-	-0.3 °C	-4.1 °C	-9.4 °C	-13.0 °C	-15.7 °C	-20.4 °C	-23.6 °C	-27.9 °C	Deg Fre	Eval
	Ps Accuracy	0.016854	0.012227	0.007782	0.005648	0.004404	0.002801	0.002029	0.001285	Infinity	Туре В
ပ္	Ps Resolution	0.000263	0.000191	0.000122	0.000088	0.000069	0.000044	0.000032	0.000020	Infinity	Туре В
0	Pc Accuracy	0.001580	0.001530	0.001464	0.001420	0.001387	0.001331	0.001294	0.001244	Infinity	Туре В
	Pc Resolution	0.000003	0.000003	0.000002	0.000002	0.000002	0.000002	0.000002	0.000002	Infinity	Туре В
	Combined	0.016930	0.012324	0.007919	0.005824	0.004618	0.003101	0.002407	0.001789	Infinity	
		34.6 °C	29.6 °C	22.7 °C	18.1 °C	14.6 °C	8.6 °C	4.5 °C	-1.1 °C		
	Ps Accuracy	0.022130	0.015971	0.010094	0.007292	0.005668	0.003585	0.002590	0.001635	Infinity	Туре В
ပ္	Ps Resolution	0.000346	0.000250	0.000158	0.000114	0.000089	0.000056	0.000040	0.000026	Infinity	Туре В
35	Pc Accuracy	0.002075	0.001998	0.001897	0.001831	0.001782	0.001698	0.001643	0.001570	Infinity	Туре В
	Pc Resolution	0.000004	0.000003	0.000003	0.000003	0.000003	0.000003	0.000003	0.000003	Infinity	Туре В
	Combined	0.022230	0.016097	0.010272	0.007519	0.005942	0.003968	0.003067	0.002267	Infinity	
		69.5 °C	63.1 °C	54.4 °C	48.6 °C	44.3 °C	36.7 °C	31.6 °C	24.8 °C		
	Ps Accuracy	0.028269	0.020280	0.012723	0.009149	0.007086	0.004457	0.003208	0.002017	Infinity	Туре В
ပ္	Ps Resolution	0.000442	0.000317	0.000199	0.000143	0.000111	0.000070	0.000050	0.000032	Infinity	Туре В
70	Pc Accuracy	0.002650	0.002537	0.002391	0.002295	0.002225	0.002107	0.002029	0.001927	Infinity	Туре В
	Pc Resolution	0.000005	0.000004	0.000004	0.000004	0.000004	0.000004	0.000003	0.000003	Infinity	Туре В
	Combined	0.028396	0.020441	0.012947	0.009433	0.007428	0.004931	0.003796	0.002790	Infinity	

Table 2



Standard Pressure Uncertainty Components of Dew Point Temperature (°C)

Figure 2

The standard Frost Point Temperature uncertainties, uT_F , components calculated using equation 11 from the associated individual pressure components are summarized in Table 3 and Figure 3.

	Standard Pressure Uncertainty Components of Frost Point Temperature (*C) Saturation Pressure Range (psia), Chamber pressure = 14.7 psia											
		S	Saturation	Pressure F	Range (psia	ı), Chambe	er pressure	= 14.7 psi	a	of 1	u	
Saturation	Description	15	20	30	40	50	75	100	150	rees (luatic	
Temperature		-0.2 °C	-3.7 °C	-8.4 °C	-11.6 °C	-14.0 °C	-18.3 °C	-21.2 °C	-25.2 °C	Deg	Eval	
	Ps Accuracy	0.014875	0.010863	0.006974	0.005092	0.003988	0.002555	0.001861	0.001187	Infinity	Туре В	
ပ္	Ps Resolution	0.000232	0.000170	0.000109	0.000080	0.000062	0.000040	0.000029	0.000019	Infinity	Туре В	
0	Pc Accuracy	0.001395	0.001359	0.001312	0.001280	0.001256	0.001215	0.001186	0.001149	Infinity	Туре В	
	Pc Resolution	0.000002	0.000002	0.000002	0.000002	0.000002	0.000002	0.000002	0.000002	Infinity	Туре В	
	Combined	0.014942	0.010949	0.007097	0.005251	0.004181	0.002830	0.002207	0.001652	Infinity		
									-0.9 °C			
	Ps Accuracy								0.001445	Infinity	Туре В	
ပ္	Ps Resolution								0.000023	Infinity	Туре В	
35	Pc Accuracy								0.001387	Infinity	Туре В	
	Pc Resolution								0.000002	Infinity	Туре В	
	Combined								0.002003	Infinity		
	Ps Accuracy									Infinity	Туре В	
ပ္	Ps Resolution									Infinity	Туре В	
70	Pc Accuracy									Infinity	Туре В	
	Pc Resolution									Infinity	Туре В	
	Combined									Infinity		

Note: Any frost point value that is not possible is grayed out of the following table.



Standard Pressure Uncertainty Components of Frost Point Temperature (°C)

Figure 3

3.2 Temperature Uncertainty Contribution

The temperature terms, T_c or T_s , in a two-pressure humidity generator are another major contributor of uncertainty and are used mathematically to calculate saturation vapor pressures. The Model 2900 humidity generator uses one temperature probe to measure the saturation temperature and another temperature probe to measure the chamber temperature. In this design, each temperature probe contributes its own uncertainty to the overall system and will be addressed independent of one another.

3.2.1 Saturation Temperature Uncertainty Contribution

The saturation temperature uncertainty contribution in terms of relative humidity can be determined by the partial numeric differential of the RH equation with respect to saturation temperature, multiplied by the uncertainty of the saturation temperature component. The equation for this becomes

$$uRH_{[component]} = \frac{\partial}{\partial T_s} \left[\frac{e_s(T_s) \cdot f(T_s, P_s)}{e_s(T_c) \cdot f(T_c, P_c)} \cdot \frac{P_c}{P_s} \cdot \eta_s \right] \cdot uT_{s[component]}$$
(15)

uRH_[component] = Saturation Temperature component uncertainty in terms of percent relative humidity.

 $uT_{S[component]}$ = Saturation Temperature component uncertainty in terms of temperature.

The saturation temperature uncertainty contribution in terms of dew or frost point temperature can be determined by the partial numeric differential of the iterative dew or frost point equation with respect to saturation temperature, multiplied by the uncertainty of the saturation temperature component. The equations for these become

$$\mathbf{u}\mathbf{T}_{\mathrm{D[component]}} = \frac{\partial}{\partial T_{S}} \left[e_{W}(T_{D}) \cdot f(T_{D}, P_{C}) = f(T_{S}, P_{S}) \cdot e(T_{S}) \cdot \frac{P_{C}}{P_{S}} \right] \cdot \mathbf{u}\mathbf{T}_{\mathrm{S}[component]}$$
(16)

$$\mathbf{u}\mathbf{T}_{\mathrm{F[component]}} = \frac{\partial}{\partial T_{S}} \left[e_{I}(T_{F}) \cdot f(T_{F}, P_{C}) = f(T_{S}, P_{S}) \cdot e(T_{S}) \cdot \frac{P_{C}}{P_{S}} \right] \cdot \mathbf{u}\mathbf{T}_{\mathrm{S}\ [component]}$$
(17)

 $uT_{D[component]} = Saturation Temperature component uncertainty in terms of dew point temperature.$ $<math>uT_{F[component]} = Saturation Temperature component uncertainty in terms of frost point temperature$ $<math>uT_{S[component]} = Saturation Temperature component uncertainty in terms of temperature.$

3.2.1.1 Saturation Temperature Measurement Uncertainty Component

Temperature measurement accuracy of Model 2900 humidity generator's saturation temperature probe encompasses 7 separate components that are listed and combined in Table 4.

	Model 29	00 Temperature C	components of Unc	ertainty	
Description	Uncertainty (±)	k=	Distribution	Degrees of Freedom	Evaluation
Standard	0.02	2	Normal	Infinity	Туре В
Resolution	0.0000625849	1	Resolution	Infinity	Туре В
Offset Error	0.00237	1	Rectangular	Infinity	Туре В
Gain Error	0.00002765	1	Rectangular	Infinity	Туре В
Hysteresis	0.015	1	Rectangular	Infinity	Туре В
Self-Heating	0.003	1	Rectangular	Infinity	Туре В
Fluid Control Stability	0.002	1	Normal	Infinity	Туре А
	·	Con	mbined Standard U	Incertainty (±):	0.01356
			Effective Degr	rees of Freedom:	Infinity
				Confidence:	95.45%
				k:	2
		Exp	anded Combined U	Incertainty (±):	0.02712

Table 4

Using the expanded result from table 4 and taking a conservative approach that is based on a rectangular distribution, the uncertainty component of saturation temperature accuracy is then

 $uT_{s[accuracy]} = 0.027 \text{ °C} / \sqrt{3} (DOF=infinite)$

resulting in

 $uT_{s[accuracy]} = 0.031 \text{ °C}$ (using a coverage factor, k=2, at an approximate level of confidence of 95%)

3.2.2 Chamber Temperature Uncertainty Contribution

The chamber temperature uncertainty contribution in terms of relative humidity can be determined by the partial numeric differential of the RH equation with respect to chamber temperature, multiplied by the uncertainty of the chamber temperature component. The equation for this becomes

$$uRH_{[component]} = \frac{\partial}{\partial T_C} \left[\frac{e_S(T_S) \cdot f(T_S, P_S)}{e_S(T_C) \cdot f(T_C, P_C)} \cdot \frac{P_C}{P_S} \cdot \eta_S \right] \cdot uT_{C[component]}$$
(18)

uRH_[component] = Chamber Temperature component uncertainty in terms of percent relative humidity.

 $uT_{C[component]}$ = Chamber Temperature component uncertainty in terms of temperature.

Examining equations 3 and 4, dew and frost point equations, we see that the chamber temperature has no component and therefore no uncertainty contribution to the generated dew or frost point temperatures.

3.2.2.1 Chamber Temperature Measurement Uncertainty Component

Temperature measurement accuracy of Model 2900 humidity generator's chamber temperature probe encompasses 7 separate components that are the same as those listed in Table 4. Using the expanded result from table 4 and taking a conservative approach that is based on a rectangular distribution, the uncertainty component of chamber temperature accuracy is then

$$uT_{c[accuracy]} = 0.027 \text{ °C} / \sqrt{3} \text{ (DOF=infinite)}$$

resulting in

 $uT_{c[accuracy]} = 0.031 \text{ °C}$ (using a coverage factor, k=2, at an approximate level of confidence of 95%)

3.2.2.2 Chamber Temperature Uniformity Uncertainty Component

The 2900 operates by generating the %RH setpoint based on pressure and temperatures which include the chamber temperature probe. This means any temperature difference in the chamber is automatically compensated by the system based on the actual chamber temperature probe reading. In scenarios where the device under test is not bundled with the chamber temperature probe or when there are multiple devices under test in the chamber then temperature gradients within the chamber can contribute to the overall %RH uncertainty of the generator. Using the expanded result from the "Model 2900 Chamber Temperature Uniformity Analysis"^[9] that is based on a rectangular distribution, the uncertainty component of chamber temperature uniformity is then

$$uT_{c[uniformity]} = 0.03 \text{ °C} / \sqrt{3} (DOF=infinite)$$

Different door configurations add a non-uniformity contributor due to the different material's thermal insulator properties. Using the expanded result from the "Model 2900 Chamber Temperature Uniformity Analysis" ^[9] that is based on a rectangular distribution, the uncertainty component of chamber temperature non-uniformity is then

 $uT_{c[non-uniformity]} = (0.00034 * |Tc|) °C / \sqrt{3} (DOF=infinite)$

where Tc is the chamber temperature in °C.

3.2.3 Temperature Uncertainty Contribution Summary

The standard uncertainties, uRH, components calculated using equations 15 and 18 from the associated individual temperature components previously shown are summarized in Table 5 and Figure 4.

		Sta	andard Ten	nperature U	Incertainty	Componen	nts of RH (S	%)			
		\$	Saturation	Pressure I	Range (psia	ı), Chambe	er pressure	= 14.7 psia	a	of 1	u
Saturation	Description	15	20	30	40	50	75	100	150	rees (uatic
Iemperature		98.0%RH	73.6%RH	49.2%RH	37.0%RH	29.6%RH	19.9%RH	15.0%RH	10.1%RH	Deg	Eval
	Ts Accuracy	0.110996	0.083335	0.055673	0.041843	0.033544	0.022480	0.016949	0.011418	Infinity	Туре В
U	Tc Accuracy	0.110997	0.083348	0.055698	0.041874	0.033579	0.022521	0.016992	0.011464	Infinity	Туре В
ů	Tc Uniformity	0.123330	0.092608	0.061887	0.046527	0.037310	0.025023	0.018880	0.012738	Infinity	Туре В
	Tc Non- Uniformity	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Infinity	Type B
	Combined	0.199627	0.149893	0.100159	0.075292	0.060373	0.040481	0.030536	0.020593	Infinity	
		98.0%RH	73.6%RH	49.1%RH	36.9%RH	29.6%RH	19.8%RH	14.9%RH	10.0%RH		
	Ts Accuracy	0.084562	0.063476	0.042386	0.031840	0.025512	0.017075	0.012856	0.008638	Infinity	Туре В
ပ္	Tc Accuracy	0.084563	0.063481	0.042398	0.031856	0.025531	0.017097	0.012881	0.008665	Infinity	Туре В
35	Tc Uniformity	0.093958	0.070534	0.047109	0.035395	0.028367	0.018997	0.014312	0.009627	Infinity	Туре В
	Tc Non- Uniformity	0.037270	0.027979	0.018686	0.014040	0.011252	0.007535	0.005677	0.003819	Infinity	Type B
	Combined	0.156585	0.117545	0.078502	0.058979	0.047265	0.031647	0.023838	0.016030	Infinity	
		98.0%RH	73.6%RH	49.2%RH	36.9%RH	29.6%RH	19.8%RH	14.9%RH	10.0%RH		
	Ts Accuracy	0.066087	0.049661	0.033192	0.024941	0.019985	0.013371	0.010061	0.006750	Infinity	Туре В
ပ္	Tc Accuracy	0.066083	0.049622	0.033145	0.024900	0.019951	0.013350	0.010049	0.006748	Infinity	Туре В
20	Tc Uniformity	0.073425	0.055135	0.036827	0.027666	0.022168	0.014834	0.011166	0.007497	Infinity	Туре В
	Tc Non- Uniformity	0.058251	0.043741	0.029216	0.021949	0.017586	0.011768	0.008858	0.005948	Infinity	Туре В
	Combined	0.132359	0.099407	0.066409	0.049892	0.039977	0.026749	0.020133	0.013516	Infinity	

Table 5



Standard Temperature Uncertainty Components of RH (%)

Figure 4

The standard uncertainties, uTD, components calculated using equation 16 from the associated individual temperature components previously shown are summarized in Table 6 and Figure 5.

	Sta	undard Ten	perature U	Incertainty	Compone	nts of Dew	Point Tem	perature (•	<i>C</i>)		
		S	Saturation	Pressure F	Range (psia	ı), Chambe	er pressure	e = 14.7 psi	a	of 1	u
Saturation	Description	15	20	30	40	50	75	100	150	rees (luatic
Temperature		-0.3 °C	-4.1 °C	-9.4 °C	-13.0 °C	-15.7 °C	-20.4 °C	-23.6 °C	-27.9 °C	Deg Fre	Eval
	Ts Accuracy	0.015553	0.015061	0.014408	0.013972	0.013648	0.013088	0.012712	0.012209	Infinity	Type B
U	Tc Accuracy	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Infinity	Туре В
ů	Tc Uniformity	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Infinity	Туре В
	Tc Non- Uniformity	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Infinity	Type B
	Combined	0.015553	0.015061	0.014408	0.013972	0.013648	0.013088	0.012712	0.012209	Infinity	
		34.6 °C	29.6 °C	22.7 °C	18.1 °C	14.6 °C	8.6 °C	4.5 °C	-1.1 °C		-
	Ts Accuracy	0.015547	0.014971	0.014215	0.013715	0.013346	0.012714	0.012293	0.011736	Infinity	Type B
ပ္	Tc Accuracy	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Infinity	Type B
35	Tc Uniformity	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Infinity	Type B
	Tc Non- Uniformity	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Infinity	Туре В
	Combined	0.015547	0.014971	0.014215	0.013715	0.013346	0.012714	0.012293	0.011736	Infinity	
		69.5 °C	63.1 °C	54.4 °C	48.6 °C	44.3 °C	36.7 °C	31.6 °C	24.8 °C		_
	Ts Accuracy	0.015540	0.014879	0.014023	0.013463	0.013053	0.012355	0.011895	0.011289	Infinity	Туре В
ပ္	Tc Accuracy	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Infinity	Type B
20	Tc Uniformity	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Infinity	Type B
	Tc Non- Uniformity	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Infinity	Туре В
	Combined	0.015540	0.014879	0.014023	0.013463	0.013053	0.012355	0.011895	0.011289	Infinity	



Standard Temperature Uncertainty Components of Dew Point Temperature (°C)

Figure 5

The standard uncertainties, uT_F , components calculated using equation 17 from the associated individual temperature components previously shown are summarized in Table 7 and Figure 7.

	Standard Temperature Uncertainty Components of Frost Point Temperature (°C) Saturation Pressure Range (psia), Chamber pressure = 14.7 psia												
		8	Saturation	Pressure F	Range (psia	ı), Chambo	er pressure	e = 14.7 psi	a	of 1	u		
Saturation	Description	15	20	30	40	50	75	100	150	rees (luatio		
Temperature		-0.2 °C	-3.7 °C	-8.4 °C	-11.6 °C	-14.0 °C	-18.3 °C	-21.2 °C	-25.2 °C	Deg	Eval		
	Ts Accuracy	0.013730	0.013380	0.012913	0.012596	0.012358	0.011942	0.011659	0.011274	Infinity	Type B		
U	Tc Accuracy	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Infinity	Туре В		
ů	Tc Uniformity	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Infinity	Туре В		
	Tc Non- Uniformity	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	Infinity	Туре В		
	Combined	0.013730	0.013380	0.012913	0.012596	0.012358	0.011942	0.011659	0.011274	Infinity			
									-0.9 °C		-		
	Ts Accuracy								0.010372	Infinity	Type B		
ပ္	Tc Accuracy								0.0	Infinity	Type B		
35	Tc Uniformity								0.0	Infinity	Type B		
	Tc Non- Uniformity								0.0	Infinity	Туре В		
	Combined								0.010372	Infinity			
											-		
	Ts Accuracy									Infinity	Type B		
ပ္	Tc Accuracy									Infinity	Type B		
70	Tc Uniformity									Infinity	Type B		
	Tc Non- Uniformity									Infinity	Туре В		
	Combined									Infinity			

Note: Any frost point value that is not possible is grayed out of the following table.



Standard Temperature Uncertainty Components of Frost Point Temperature (°C)

3.3 Equation Uncertainty Contribution

The equations used to calculate the saturation vapor pressure at a given temperature and its enhancement factor at the same temperature and given pressure have published uncertainties as determined by the author or authors of the equations. These equations are used throughout the Relative Humidity, Dew point and Frost point equations and therefore contribute their own uncertainty to the overall system.

3.3.1 Saturation Vapor Pressure Equation Uncertainty Component

The saturation vapor pressure is the partial pressure of the water vapor at a given temperature with respect to ice or water. The saturation vapor pressure is dependent on temperature only and is computed with the Wexler's^[4] saturation vapor pressure equation. Wexler^[4] also list a table of uncertainties at various temperatures for his saturation vapor pressure equation. These uncertainty values are interpolated to determine the saturation vapor pressure equation uncertainty component for a given temperature.

3.3.2 Enhancement Factor Equation Uncertainty Component

Enhancement factors are slight correction factors used to account for the non-ideal behavior of water vapor when admixed with other gases. The enhancement factor is dependent on both temperature and pressure and is computed with Greenspan's^[5] enhancement factor equation. Wexler and R.W. Hyland^[8] list a table of uncertainties for various temperatures and pressures for the enhancement factor equation. These uncertainty values are interpolated to determine the enhancement factors equation uncertainty component for a given temperature and pressure.

3.3.3 Equation Uncertainty Contribution Summary

The standard uncertainties, uRH, components calculated using the associated equation uncertainty tables mentioned above are summarized in Table 8 and Figure 7.

	Standard Equation Uncertainty Components of RH (%) Saturation Pressure Range (psia), Chamber pressure = 14.7 psia												
		:	Saturation	Pressure H	Range (psia	ı), Chambe	er pressure	= 14.7 psia	a	of 1	u		
Saturation	Description	15	20	30	40	50	75	100	150	rees o	luatic		
Temperature		98.0%RH	73.6%RH	49.2%RH	37.0%RH	29.6%RH	19.9%RH	15.0%RH	10.1%RH	Deg Fre	Eval		
	SVP@Ts	0.001562	0.001172	0.000781	0.000586	0.000469	0.000312	0.000234	0.000156	Infinity	Туре В		
ပ္	F@Ts,Ps	0.010136	0.010148	0.010172	0.010197	0.010221	0.010249	0.010060	0.009967	Infinity	Туре В		
Õ	SVP@Tc	0.001563	0.001173	0.000784	0.000589	0.000473	0.000317	0.000239	0.000161	Infinity	Туре В		
	F@Tc,Pc	0.009933	0.007459	0.004985	0.003747	0.003005	0.002015	0.001521	0.001026	Infinity	Туре В		
	Combined	0.014363	0.012703	0.011382	0.010895	0.010675	0.010454	0.010180	0.010022	Infinity			
		98.0%RH	73.6%RH	49.1%RH	36.9%RH	29.6%RH	19.8%RH	14.9%RH	10.0%RH		-		
	SVP@Ts	0.008209	0.006157	0.004105	0.003079	0.002463	0.001642	0.001231	0.000821	Infinity	Туре В		
ပ္	F@Ts,Ps	0.007623	0.007783	0.007951	0.008042	0.008103	0.008214	0.008376	0.008575	Infinity	Туре В		
35	SVP@Tc	0.008210	0.006163	0.004116	0.003093	0.002479	0.001660	0.001251	0.000841	Infinity	Туре В		
	F@Tc,Pc	0.007458	0.005599	0.003739	0.002810	0.002252	0.001508	0.001136	0.000764	Infinity	Туре В		
	Combined	0.015765	0.012955	0.010535	0.009572	0.009107	0.008672	0.008633	0.008688	Infinity			
		98.0%RH	73.6%RH	49.2%RH	36.9%RH	29.6%RH	19.8%RH	14.9%RH	10.0%RH		-		
	SVP@Ts	0.002050	0.001539	0.001027	0.000771	0.000617	0.000411	0.000308	0.000206	Infinity	Туре В		
ပ္	F@Ts,Ps	0.003652	0.004423	0.005200	0.005593	0.005833	0.006177	0.006448	0.006745	Infinity	Туре В		
70	SVP@Tc	0.002050	0.001539	0.001028	0.000772	0.000619	0.000414	0.000312	0.000209	Infinity	Туре В		
	F@Tc,Pc	0.003518	0.002642	0.001765	0.001326	0.001062	0.000711	0.000535	0.000359	Infinity	Туре В		
	Combined	0.005841	0.005593	0.005680	0.005851	0.005993	0.006245	0.006485	0.006760	Infinity			



Figure 7

		Standard	Equation U	U ncertainty	Componer	nts of Dew	Point Temp	oerature (•C	<i>C</i>)		
		5	Saturation	Pressure H	Range (psia), Chambe	er pressure	= 14.7 psia	a	of 1	u
Saturation	Description	15	20	30	40	50	75	100	150	rees (uatio
Temperature		-0.3 °C	-4.1 °C	-9.4 °C	-13.0 °C	-15.7 °C	-20.4 °C	-23.6 °C	-27.9 °C	Degi Fre	Eval
	SVP@Ts	0.000219	0.000212	0.000202	0.000196	0.000191	0.000182	0.000176	0.000167	Infinity	Туре В
ပ္	F@Ts,Ps	0.001420	0.001834	0.002633	0.003405	0.004159	0.005967	0.007545	0.010657	Infinity	Туре В
õ	SVP@Td	0.000219	0.000212	0.000203	0.000197	0.000192	0.000184	0.000179	0.000172	Infinity	Туре В
	F@Td,Pc	0.001411	0.001630	0.001902	0.002068	0.002184	0.002349	0.002285	0.002200	Infinity	Туре В
	Combined	0.002026	0.002472	0.003260	0.003993	0.004705	0.006417	0.007887	0.010885	Infinity	
		34.6 °C	29.6 °C	22.7 °C	18.1 °C	14.6 °C	8.6 °C	4.5 °C	-1.1 °C		-
	SVP@Ts	0.001509	0.001452	0.001377	0.001326	0.001288	0.001223	0.001178	0.001115	Infinity	Туре В
ပ္	F@Ts,Ps	0.001401	0.001836	0.002667	0.003464	0.004239	0.006116	0.008009	0.011650	Infinity	Туре В
35	SVP@Td	0.001541	0.001905	0.001997	0.001586	0.001295	0.000820	0.000522	0.000218	Infinity	Туре В
	F@Td,Pc	0.001338	0.000923	0.001439	0.001607	0.001565	0.001493	0.001446	0.001457	Infinity	Туре В
	Combined	0.002899	0.003156	0.003881	0.004342	0.004874	0.006466	0.008240	0.011796	Infinity	
		69.5 °C	63.1 °C	54.4 °C	48.6 °C	44.3 °C	36.7 °C	31.6 °C	24.8 °C		-
	SVP@Ts	0.000482	0.000461	0.000434	0.000416	0.000403	0.000380	0.000365	0.000344	Infinity	Туре В
ပ္	F@Ts,Ps	0.000859	0.001325	0.002197	0.003019	0.003810	0.005708	0.007623	0.011280	Infinity	Туре В
70	SVP@Td	0.000485	0.000507	0.000739	0.000936	0.001033	0.001382	0.001761	0.002186	Infinity	Туре В
	F@Td,Pc	0.000844	0.001025	0.001063	0.001158	0.001542	0.001550	0.001042	0.001291	Infinity	Туре В
	Combined	0.001385	0.001810	0.002587	0.003392	0.004257	0.006086	0.007901	0.011568	Infinity	

The standard uncertainties, uT_D , components calculated using the associated equation uncertainty tables mentioned above are summarized in Table 9 and Figure 8.



Standard Equation Uncertainty Components of Dew Point Temperature (°C)

Figure 8

The standard uncertainties, uT_F , components calculated using the associated equation uncertainty tables mentioned above are summarized in Table 10 and Figure 9.

Note: Any frost point value that is not possible is grayed out of the following table.

Standard Equation Uncertainty Components of Frost Point Temperature (°C) Saturation Pressure Range (psia), Chamber pressure = 14.7 psia 2											
		:	Saturation	Pressure I	Range (psia	ı), Chambe	er pressure	= 14.7 psia	a	l f	u
Saturation	Description	15	20	30	40	50	75	100	150	rees (uatic
Temperature		-0.2 °C	-3.7 °C	-8.4 °C	-11.6 °C	-14.0 °C	-18.3 °C	-21.2 °C	-25.2 °C	Deg Fre	Eval
	SVP@Ts	0.000193	0.000188	0.000181	0.000176	0.000173	0.000166	0.000161	0.000154	Infinity	Туре В
ပ္	F@Ts,Ps	0.001254	0.001629	0.002359	0.003070	0.003766	0.005444	0.006920	0.009841	Infinity	Туре В
0	SVP@Tf	0.000353	0.002536	0.005335	0.006990	0.008070	0.009865	0.010939	0.012163	Infinity	Туре В
	F@Tf,Pc	0.001244	0.001420	0.001644	0.001785	0.001886	0.002052	0.002094	0.002030	Infinity	Туре В
	Combined	0.001811	0.003337	0.006063	0.007843	0.009104	0.011454	0.013114	0.015777	Infinity	
									-0.9 °C		
	SVP@Ts								0.000986	Infinity	Туре В
ပိ	F@Ts,Ps								0.010297	Infinity	Туре В
35	SVP@Tf								0.000804	Infinity	Туре В
	F@Tf,Pc								0.001280	Infinity	Туре В
	Combined								0.010453	Infinity	
	SVP@Ts									Infinity	Туре В
ပ္	F@Ts,Ps									Infinity	Туре В
70	SVP@Tf									Infinity	Type B
	F@Tf,Pc									Infinity	Туре В
	Combined									Infinity	



Standard Equation Uncertainty Components of Frost Point Temperature (°C)

Figure 9

3.4 Saturator Efficiency Uncertainty Contribution

All two-pressure humidity generators rely on the ability of the saturator to fully saturate the gas with water vapor as it passes from inlet to outlet. The Model 2900 humidity generator incorporates a presaturator device along with the saturator to assure the full saturation of the gas with water vapor. Why this design helps assure 100% saturation of the gas, there may still be small amounts of uncertainty.

Based on engineering research and development work on the Model 2900, the uncertainty component of % efficiency of saturation is determined to be

$$\eta_{s} = 99.93\%$$

The standard uncertainties, uRH, components calculated using the above associated % efficiency component are summarized in Table 11 and Figure 10.

	Standard Saturator Efficiency Uncertainty Components of RH (%)												
		:	Saturation	Pressure H	Range (psia	ı), Chambe	er pressure	= 14.7 psia	a	of 1	u		
Saturation	Description	15	20	30	40	50	75	100	150	rees (uatic		
Temperature		98.0%RH	73.6%RH	49.2%RH	37.0%RH	29.6%RH	19.9%RH	15.0%RH	10.1%RH	Deg Fre	Eval		
D. 0	η_S	0.068605	0.051515	0.034426	0.025881	0.020755	0.013920	0.010502	0.007086	Infinity	Type B		
	Combined	0.068605	0.051515	0.034426	0.025881	0.020755	0.013920	0.010502	0.007086	Infinity			
		98.0%RH	73.6%RH	49.1%RH	36.9%RH	29.6%RH	19.8%RH	14.9%RH	10.0%RH				
35 °C	η_S	0.068604	0.051501	0.034396	0.025844	0.020713	0.013871	0.010450	0.007029	Infinity	Type B		
	Combined	0.068604	0.051501	0.034396	0.025844	0.020713	0.013871	0.010450	0.007029	Infinity			
		98.0%RH	73.6%RH	49.2%RH	36.9%RH	29.6%RH	19.8%RH	14.9%RH	10.0%RH				
70 °C	η_S	0.068606	0.051516	0.034410	0.025850	0.020713	0.013860	0.010433	0.007005	Infinity	Type B		
	Combined	0.068606	0.051516	0.034410	0.025850	0.020713	0.013860	0.010433	0.007005	Infinity			

Table 11



Standard Saturator Efficiency Uncertainty Components of RH (%)

Figure 10

The standard uncertainties, uT_D , components calculated using the above associated % efficiency component are summarized in Table 12 and Figure 11.

	Standard Saturator Efficiency Uncertainty Components of Dew Point Temperature (*C)											
		:	Saturation	Pressure H	Range (psia	ı), Chambe	er pressure	= 14.7 psia	a	of 1	u	
Saturation	Description	15	20	30	40	50	75	100	150	rees (uatic	
Temperature		-0.3 °C	-4.1 °C	-9.4 °C	-13.0 °C	-15.7 °C	-20.4 °C	-23.6 °C	-27.9 °C	Degi Fre	Eval	
D. 0	η_{S}	0.009613	0.009310	0.008909	0.008642	0.008444	0.008104	0.007877	0.007576	Infinity	Туре В	
	Combined	0.009613	0.009310	0.008909	0.008642	0.008444	0.008104	0.007877	0.007576	Infinity		
		34.6 °C	29.6 °C	22.7 °C	18.1 °C	14.6 °C	8.6 °C	4.5 °C	-1.1 °C			
35 °C	η_{S}	0.012613	0.012147	0.011536	0.011132	0.010835	0.010328	0.009992	0.009551	Infinity	Type B	
	Combined	0.012613	0.012147	0.011536	0.011132	0.010835	0.010328	0.009992	0.009551	Infinity		
		69.5 °C	63.1 °C	54.4 °C	48.6 °C	44.3 °C	36.7 °C	31.6 °C	24.8 °C			
70 °C	η_S	0.016132	0.015435	0.014538	0.013954	0.013528	0.012807	0.012334	0.011716	Infinity	Type B	
	Combined	0.016132	0.015435	0.014538	0.013954	0.013528	0.012807	0.012334	0.011716	Infinity		

Table 12



Standard Saturator Efficiency Uncertainty Components of Dew Point Temperature (°C)

Figure 11

The standard uncertainties, uT_F , components calculated using the above associated % efficiency component are summarized in Table 13 and Figure 12.

Note: Any frost point value that is not possible is grayed out of the following table.

	Standard Saturator Efficiency Uncertainty Components of Frost Point Temperature (*C)													
		1	of 1	u										
Saturation Temperature	Description	15	20	30	40	50	75	100	150	rees (uatic			
		-0.2 °C	-3.7 °C	-8.4 °C	-11.6 °C	-14.0 °C	-18.3 °C	-21.2 °C	-25.2 °C	Degi Fre	Eval			
ວ. 0	η_S	0.008484	0.008271	0.007985	0.007791	0.007646	0.007394	0.007224	0.006996	Infinity	Туре В			
	Combined	0.008484	0.008271	0.007985	0.007791	0.007646	0.007394	0.007224	0.006996	Infinity				
									-0.9 °C					
35 °C	η_S								0.008441	Infinity	Туре В			
	Combined								0.008441	Infinity				
70 °C	η_S									Infinity	Туре В			
	Combined									Infinity				



Standard Saturator Efficiency Uncertainty Components of Frost Point Temperature (°C)

Figure 12

4.0 Combined Standard and Expanded Uncertainty

The combined standard uncertainty is obtained by the statistical combination of the individual standard uncertainty components of pressure, temperature, and equation in terms of relative humidity, dew point or frost point. Utilizing a confidence level of 95.45% and a coverage factor k=2, the expanded uncertainty, U, is expressed by multiplying the combined standard uncertainty by the coverage factor as show in the following formula

$$\mathbf{U} = \mathbf{k} * \mathbf{u}_{\mathbf{c}} \tag{19}$$

Using equations 6 and 19, the combined individual standard uncertainty components for pressure, temperature, equation and saturator efficiency, the total combined standard uncertainty (u) and the total combined expanded uncertainty (U) in terms of relative humidity RH (%) are summarized in Table 14 and Figure 13.

Uncertainty Components of RH (%)												
		1	Saturation	Pressure H	Range (psia), Chambe	er pressure	= 14.7 psia	a	of 1		
Saturation	Description	15	20	30	40	50	75	100	150	rees (
Temperature		98.0%RH	73.6%RH	49.2%RH	37.0%RH	29.6%RH	19.9%RH	15.0%RH	10.1%RH	Deg Fre		
	Pressure	0.120822	0.068193	0.030601	0.017443	0.011351	0.005327	0.003210	0.001674	Infinity		
	Temperature	0.199627	0.149893	0.100159	0.075292	0.060373	0.040481	0.030536	0.020593	Infinity		
	Equation	0.014363	0.012703	0.011382	0.010895	0.010675	0.010454	0.010180	0.010022	Infinity		
0 °C	Saturator Efficiency	0.068605	0.051515	0.034426	0.025881	0.020755	0.013920	0.010502	0.007086	Infinity		
	Combined	0.243643	0.173013	0.110828	0.082230	0.065715	0.044386	0.034010	0.024032	Infinity		
	Expanded (k=2)	0.487285	0.346025	0.221657	0.164460	0.131429	0.088772	0.068020	0.048064			
		98.0%RH	73.6%RH	49.1%RH	36.9%RH	29.6%RH	19.8%RH	14.9%RH	10.0%RH			
	Pressure	0.120915	0.068249	0.030627	0.017457	0.011359	0.005329	0.003208	0.001669	Infinity		
	Temperature	0.156585	0.117545	0.078502	0.058979	0.047265	0.031647	0.023838	0.016030	Infinity		
U	Equation	0.015765	0.012955	0.010535	0.009572	0.009107	0.008672	0.008633	0.008688	Infinity		
35 °(Saturator Efficiency	0.068604	0.051501	0.034396	0.025844	0.020713	0.013871	0.010450	0.007029	Infinity		
	Combined	0.209987	0.145928	0.091622	0.067401	0.053619	0.036021	0.027609	0.019612	Infinity		
	Expanded (k=2)	0.419973	0.291856	0.183245	0.134801	0.107238	0.072042	0.055218	0.039224			
		98.0%RH	73.6%RH	49.2%RH	36.9%RH	29.6%RH	19.8%RH	14.9%RH	10.0%RH			
	Pressure	0.120759	0.068225	0.030644	0.017474	0.011372	0.005335	0.003210	0.001667	Infinity		
	Temperature	0.132359	0.099407	0.066409	0.049892	0.039977	0.026749	0.020133	0.013516	Infinity		
0	Equation	0.005841	0.005593	0.005680	0.005851	0.005993	0.006245	0.006485	0.006760	Infinity		
). OL	Saturator Efficiency	0.068606	0.051516	0.034410	0.025850	0.020713	0.013860	0.010433	0.007005	Infinity		
	Combined	0.191944	0.131231	0.081028	0.059136	0.046823	0.031227	0.023802	0.016740	Infinity		
	Expanded (k=2)	0.383888	0.262463	0.162055	0.118271	0.093646	0.062453	0.047605	0.033480			

Table 14

Uncertainty Analysis of the Thunder Scientific Model 2900 Two-Pressure Humidity Generator (revision 1) Copyright © 2018, Thunder Scientific Corporation. All Rights Reserved. Document: Model_2900_Uncertainty_Analysis (Rev3) Author: Michael Hamilton Date: February 2019

Uncertainty Components of RH (%)



Figure 13

Using equations 7 and 19, the combined individual standard uncertainty components for pressure, temperature, equation and saturator efficiency, the total combined standard uncertainty (u) and the total combined expanded uncertainty (U) in terms of dew point temperature Td (°C) are summarized in Table 15 and Figure 14.

Uncertainty Components of Dew Point Temperature (*C)												
		S	aturation	Pressure F	Range (psia), Chambe	er pressure	e = 14.7 psi	a	of 1		
Saturation	Description	15	20	30	40	50	75	100	150	rees (
Temperature		-0.3 °C	-4.1 °C	-9.4 °C	-13.0 °C	-15.7 °C	-20.4 °C	-23.6 °C	-27.9 °C	Deg		
	Pressure	0.016930	0.012324	0.007919	0.005824	0.004618	0.003101	0.002407	0.001789	Infinity		
	Temperature	0.012673	0.012272	0.011740	0.011384	0.011120	0.010664	0.010358	0.009948	Infinity		
	Equation	0.002026	0.002472	0.003260	0.003993	0.004705	0.006417	0.007887	0.010885	Infinity		
0 0	Saturator Efficiency	0.009613	0.009310	0.008909	0.008642	0.008444	0.008104	0.007877	0.007576	Infinity		
	Combined	0.023318	0.019881	0.017045	0.015942	0.015441	0.015172	0.015406	0.016675	Infinity		
	Expanded (k=2)	0.046636	0.039763	0.034091	0.031885	0.030882	0.030344	0.030811	0.033349			
		34.6 °C	29.6 °C	22.7 °C	18.1 °C	14.6 °C	8.6 °C	4.5 °C	-1.1 °C			
	Pressure	0.022230	0.016097	0.010272	0.007519	0.005942	0.003968	0.003067	0.002267	Infinity		
	Temperature	0.012668	0.012199	0.011583	0.011175	0.010874	0.010359	0.010017	0.009563	Infinity		
O	Equation	0.002899	0.003156	0.003881	0.004342	0.004874	0.006466	0.008240	0.011796	Infinity		
35 °(Saturator Efficiency	0.012613	0.012147	0.011536	0.011132	0.010835	0.010328	0.009992	0.009551	Infinity		
	Combined	0.028673	0.023779	0.019693	0.018006	0.017167	0.016478	0.016658	0.018082	Infinity		
	Expanded (k=2)	0.057346	0.047557	0.039386	0.036012	0.034334	0.032957	0.033316	0.036164			
		69.5 °C	63.1 °C	54.4 °C	48.6 °C	44.3 °C	36.7 °C	31.6 °C	24.8 °C			
	Pressure	0.028396	0.020441	0.012947	0.009433	0.007428	0.004931	0.003796	0.002790	Infinity		
	Temperature	0.012662	0.012124	0.011426	0.010970	0.010636	0.010067	0.009692	0.009199	Infinity		
0	Equation	0.001385	0.001810	0.002587	0.003392	0.004257	0.006086	0.007901	0.011568	Infinity		
70 °(Saturator Efficiency	0.016132	0.015435	0.014538	0.013954	0.013528	0.012807	0.012334	0.011716	Infinity		
	Combined	0.035055	0.028396	0.022721	0.020385	0.019221	0.018076	0.017970	0.019065	Infinity		
	Expanded (k=2)	0.070110	0.056792	0.045442	0.040770	0.038441	0.036151	0.035940	0.038130			

Uncertainty Components of Dew Point Temperature (°C)

Figure 14

Using equations 8 and 19, the combined individual standard uncertainty components for pressure, temperature, equation and saturator efficiency, the total combined standard uncertainty (u) and the total combined expanded uncertainty (U) in terms of frost point temperature Tf (°C) are summarized in Table 16 and Figure 15.

	Uncertainty Components of Frost Point Temperature (•C)												
		S	aturation	Pressure R	Range (psia	ı), Chambe	er pressure	e = 14.7 psi	a	of J			
Saturation	Description	15	20	30	40	50	75	100	150	rees (
Temperature		-0.2 °C	-3.7 °C	-8.4 °C	-11.6 °C	-14.0 °C	-18.3 °C	-21.2 °C	-25.2 °C	Deg Fre			
	Pressure	0.014942	0.010949	0.007097	0.005251	0.004181	0.002830	0.002207	0.001652	Infinity			
	Temperature	0.013730	0.013380	0.012913	0.012596	0.012358	0.011942	0.011659	0.011274	Infinity			
	Equation	0.001811	0.003337	0.006063	0.007843	0.009104	0.011454	0.013114	0.015777	Infinity			
0 °C	Saturator Efficiency	0.008484	0.008271	0.007985	0.007791	0.007646	0.007394	0.007224	0.006996	Infinity			
	Combined	0.022069	0.019454	0.017822	0.017562	0.017651	0.018344	0.019104	0.020681	Infinity			
	Expanded (k=2)	0.044139	0.038908	0.035645	0.035125	0.035302	0.036687	0.038207	0.041362				
									-0.9 °C				
	Pressure								0.002003	Infinity			
	Temperature								0.010372	Infinity			
O	Equation								0.010453	Infinity			
35 °(Saturator Efficiency								0.008441	Infinity			
	Combined								0.017092	Infinity			
	Expanded (k=2)								0.034183				
	Pressure									Infinity			
	Temperature									Infinity			
0	Equation									Infinity			
70 °C	Saturator Efficiency									Infinity			
	Combined									Infinity			
	Expanded (k=2)												

Note: Any frost point value that is not possible is grayed out of the following tables.

Figure 15

5.0 Summary

To simplify the %RH uncertainty results, the following uncertainty specification statement is used to describe the RH (%) uncertainty for the Model 2900:

0.5% of reading RH

(using a coverage factor, k=2, at an approximate level of confidence of 95%)

A summary of the combined expanded uncertainty (U_{RH}) and uncertainty specification for RH (%) are shown in Table 17 and Figure 16.

Expanded Uncertainty of RH (%)													
Saturation Temperature	Saturation Pressure Range (psia), Chamber pressure = 14.7 psia												
	15	20	30	40	40 50		100	150					
	98.0 %RH	73.6 %RH	49.2 %RH	37.0 %RH	29.6 %RH	19.9 %RH	15.0 %RH	10.0 %RH					
0 °C	0.487	0.346	0.222	0.164	0.131	0.089	0.068	0.048					
35 °C	0.420	0.292	0.183	0.135	0.107	0.072	0.055	0.039					
70 °C	0.384	0.262	0.162	0.118	0.094	0.062	0.048	0.033					
0.5% Specification	0.490	0.368	0.246	0.185	0.148	0.100	0.075	0.050					

Expanded Uncertainty of RH (%)

Figure 16

To simplify the Dew Point Temperature uncertainty results, the following uncertainty specification statement is used to describe the Dew Point (°C) uncertainty (U_{Td}) for the Model 2900 over the range of 0 °C to 70 °C:

0.08 °C

(using a coverage factor, k=2, at an approximate level of confidence of 95%)

A summary of the combined expanded uncertainty and uncertainty specification for Dew Point Temperature (°C) over the range of 0 to 70 °C are shown in Table 18 and Figure 17.

Expanded Uncertainty of Dew Point Temperature (*C)													
	Saturation Pressure Range (psia), Chamber pressure = 14.7 psia												
Saturation Temperature	15	20	30	40	50	75	100	150					
	34.6 °C	29.6 °C	22.7 °C	18.1 °C	14.6 °C	8.6 °C	4.5 °C						
35 °C	0.057	0.048	0.039	0.036	0.034	0.033	0.033						
	69.5 °C	63.1 °C	54.4 °C	48.6 °C	44.3 °C	36.7 °C	31.6 °C	24.8 °C					
70 °C	0.070	0.057	0.045	0.041	0.038	0.036	0.036	0.038					
0.08 Specification	0.080	0.080	0.080	0.080	0.080	0.080	0.080	0.080					

Expanded Uncertainty of Dew Point Temperature (°C)

Figure 17

To simplify the Dew/Frost Point Temperature uncertainty results, the following uncertainty specification statement is used to describe the Dew/Frost Point (°C) uncertainty (U_{Tf}) for the Model 2900 for Dew/Frost Point Temperatures below 0 °C:

0.05 °C

(using a coverage factor, k=2, at an approximate level of confidence of 95%)

A summary of the combined expanded uncertainty and uncertainty specification for Dew/Frost Point Temperature (°C) below 0 °C are shown in Table 18 and Figure 17.

	Expanded Uncertainty of Dew/Frost Point Temperature (*C)													
		Saturation Pressure Range (psia), Chamber pressure = 14.7 psia												
Saturation Temperature	15	20	30	40	50	75	100	150						
	-0.3 °C	-4.1 °C	-9.4 °C	-13.0 °C	-15.7 °C	-20.4 °C	-23.6 °C	-27.9 °C	Td					
3° 0	0.047	0.040	0.034	0.032	0.031	0.030	0.031	0.033						
	-0.2 °C	-3.7 °C	-8.4 °C	-11.6 °C	-14.0 °C	-18.3 °C	-21.2 °C	-25.2 °C	Tf					
0°C	0.041	0.036	0.032	0.032	0.032	0.034	0.036	0.039						
								-1.1 °C	Td					
35 °C								0.036						
								-0.9 °C	Tf					
35 °C								0.032						
		1	1			1	1		- 7					
0.05 Specification	0.050	0.050	0.050	0.050	0.050	0.050	0.050	0.050						

Table 19

Expanded Uncertainty of Dew/Frost Point Temperature (°C)

Figure 18

6.0 References

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